

Created 09/01/25  
Updated 09/22/25 (slides 12-15)

## Experimental sets:

$^{124}\text{Xe}(345\text{A MeV}) + \text{Be}$  : H.Suzuki et al., Prog. Theor. Exp. Phys. 2025 053D02  
 $^{78}\text{Kr}(345\text{A MeV}) + \text{Be}$  : H.Suzuki et al., Prog. Theor. Exp. Phys. 2025 053D03

Which EE model is more appropriate?

Excitation energy model "Tmean"  
LISE v.17.15.27

4. Exponential excitation-energy distribution -- L.Audirac et al., PRC88, 041602(R) (2013)

$\langle T \rangle$  - Mean Distribution Value (MeV)  $E = \Delta A (k_1 + k_2 \Delta A + k_{NZ} (\Delta N - \Delta Z))$

| $k_1$ | $k_2$  | $k_{NZ}$ | Mean Excitation Energy = |           |
|-------|--------|----------|--------------------------|-----------|
| 13.79 | -0.216 | 0        | 116.3                    | MeV       |
|       |        |          | Standard deviation =     | 36.77 MeV |

What is more suitable dimension value?

Evaporation options

Dimension of evaporation distributions [64]

What decay channels should be used? What daughter energy distribution?

Decay modes

| 1n                                  | 2n                       | 1p                                  | 2p                                  | $\alpha$                            | d                        | t                        | $^3\text{He}$            | Fission                  | Breakup                             | $\gamma$                 |
|-------------------------------------|--------------------------|-------------------------------------|-------------------------------------|-------------------------------------|--------------------------|--------------------------|--------------------------|--------------------------|-------------------------------------|--------------------------|
| <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input type="checkbox"/> | <input checked="" type="checkbox"/> | <input type="checkbox"/> |

protected mode ☐ debugging mode ☒

Mode

☐ manual ☒ auto

For "daughter" nucleus excitation energy distribution apply:

☐ energy distribution of emitted light particle (qualitatively)

☒ average energy of emitted light particle (fast) [recommended for high Z]

What are more suitable Odd/even values?

Odd-Even Delta parameters

Evaporation =  default 12

Fission =  14

## Deduction of Abrasion–Ablation (AA) Parameters and Weighted Cross Sections

### Calibration on reference beams

The AA parameters (temperature coefficients, scaling factors, etc.) were determined separately for each of the eight nuclear mass models by fitting the measured production cross sections for the reactions  $^{78}\text{Kr} + \text{Be}$ ,  $^{124}\text{Xe} + \text{Be}$ . Minimization employed the Levenberg–Marquardt algorithm with a combined  $\chi^2$ /logarithmic objective to balance absolute and relative deviations.

### Systematics for intermediate projectiles

For beams where no direct fit is possible ( $^{92}\text{Mo}$ ), the AA parameters were interpolated/extrapolated from the excitation–energy systematics as a function of projectile mass and charge, using the trends established in the calibrated systems.

### Mass-model ensemble

For each mass model, a complete set of AA parameters was thus available and used to calculate fragmentation cross sections for the beam of interest.

### Model weighting

To combine the different mass models into a single prediction, relative statistical weights were assigned according to their performance in the reference systems:  $w_i \propto 1 / (\chi^2_{^{78}\text{Kr},i} \chi^2_{^{124}\text{Xe},i})$  where  $\chi^2$  are the minimized objective values for mass model  $i$ .

### Weighted averages

The final deduced cross sections were obtained as a weighted average across the eight mass models

### Error estimation.

Cross-section uncertainties include both experimental errors and the spread among mass-model predictions, the latter quantified by the weighted variance.

### Creation of CS user file to be used in LISE<sup>++</sup>

Minimization  
value

Excitation energy parameters  
 $k_1, k_2, k_{NZ}$

Limiting temperature  
to be used  
in break-up channel

Tunneling

| date   | method | mass     | NP | s  | 2p  | mw/2t | Final  | wErr | e0     | e1       | e2       | AA-factor | Tlim<br>50 | Tlim<br>150 |  | dRauto 0 | dRauto 1  | dRauto 2  |
|--------|--------|----------|----|----|-----|-------|--------|------|--------|----------|----------|-----------|------------|-------------|--|----------|-----------|-----------|
| 29-Aug | Tmean  | frdm2012 | 32 | 12 | yes | 2t    | 3.66   | 1.00 | 11.99  | -2.5E-01 | 2.6E-01  | 1.00E+00  | 9.74E+00   | 6.00E+00    |  | 5.19E+00 | -1.32E-01 | 4.56E-02  |
| 29-Aug | Tmean  | tuyy     | 32 | 12 | yes | 2t    | 4.11   | 1.21 | 13.05  | -8.9E-02 | -3.4E-02 | 1.00E+00  | 8.79E+00   | 5.88E+00    |  | 5.18E+00 | -1.35E-01 | 5.76E-02  |
| 1-Sep  | Tmean  | hfb27    | 32 | 12 | yes | 2t    | 5.13   | 1.57 | 12.94  | -1.0E-01 | -2.6E-03 | 1.00E+00  |            |             |  | 5.65E+00 | -3.78E-02 | 3.50E-02  |
| 31-Aug | Tmean  | ws4rbf   | 32 | 10 | yes | 2t    | 5.83   | 1.78 | 13.08  | -1.1E-01 | -1.7E-02 |           |            |             |  | 5.41E+00 | -2.61E-01 | 7.47E-02  |
| 29-Aug | Tmean  | ame2020  | 32 | 12 | yes | 2t    | 7.58   | 2.22 | 12.67  | 3.8E-02  | -2.1E-01 | 1.00E+00  | 8.22E+00   | 6.31E+00    |  | 5.55E+00 | 3.65E-01  | -9.51E-02 |
| 29-Aug | Tmean  | ktyu     | 32 | 12 | yes | 2t    | 7.88   | 2.28 | 12.34  | 7.1E-03  | -2.7E-01 | 1.00E+00  | 8.27E+00   | 6.03E+00    |  | 5.28E+00 | 3.67E-02  | 1.00E-01  |
| 29-Aug | Tmean  | hfb22    | 32 | 12 | yes | 2t    | 8.67   | 2.45 | 13.29  | -8.1E-02 | -7.3E-02 | 1.00E+00  | 8.03E+00   | 5.94E+00    |  | 5.19E+00 | -1.32E-01 | 4.61E-02  |
| 29-Aug | Tmean  | unedf1   | 32 | 12 | yes | 2t    | 9.71   | 2.66 | 14.14  | -3.5E-01 | 1.7E-01  | 1.00E+00  | 8.79E+00   | 5.88E+00    |  | 6.00E+00 | -3.52E-02 | 9.80E-02  |
|        |        |          |    |    |     |       |        |      |        |          |          |           |            |             |  |          |           |           |
|        |        |          |    |    |     |       | meanW  |      | 12.693 | -0.142   | 0.048    |           | 9.045      | 5.983       |  | 5.337    | -0.086    | 0.046     |
|        |        |          |    |    |     |       | sigmaW |      | 0.217  | 0.039    | 0.064    |           | 0.283      | 0.051       |  | 0.084    | 0.052     | 0.016     |

| Line | Last | chi2<br>local | LogDif<br>local | chi2<br>total | LogDif<br>total |
|------|------|---------------|-----------------|---------------|-----------------|
| Z=30 | 18   | 0.1           | 2               | 0.2           | 10              |
| Z=30 | 18   | 0.1           | 2               | 0.2           | 10              |
| Z=30 | 21   | 0.1           | 2               | 0.1           | 5               |
| Z=30 | 21   | 0.1           | 2               | 0.1           | 5               |

Minimization  
value

Excitation energy parameters  
 $k_1, k_2, k_{NZ}$

Limiting temperature  
to be used  
in break-up channel

Tunneling

| Beam  | A   | Z  | date   | method | mass     | NP | s  | 2p  | mw/2t | Final  | wErr | e0     | e1        | e2        | AA-factor | Tlim<br>50 | Tlim<br>150 |  | dRauto 0 | dRauto 1  | dRauto 2  |
|-------|-----|----|--------|--------|----------|----|----|-----|-------|--------|------|--------|-----------|-----------|-----------|------------|-------------|--|----------|-----------|-----------|
| 124Xe | 124 | 54 | 29-Aug | Tmean  | hfb27    | 32 | 12 | yes | 2t    | 2.13   | 1.00 | 20.760 | -2.61E-01 | 1.36E-01  | 1.00E+00  | 9.23E+00   | 6.89E+00    |  | 4.94E+00 | -7.72E-02 | 4.12E-03  |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | ws4rbf   | 32 | 12 | yes | 2t    | 2.87   | 1.32 | 20.148 | -1.02E-01 | 5.39E-02  | 1.00E+00  | 8.71E+00   | 6.83E+00    |  | 5.20E+00 | -1.95E-01 | 1.93E-02  |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | unedf1   | 32 | 12 | yes | 2t    | 2.89   | 1.33 | 21.719 | -1.31E-01 | -6.61E-02 | 1.00E+00  | 8.71E+00   | 6.21E+00    |  | 5.20E+00 | -1.71E-01 | 1.81E-02  |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | ame2020  | 32 | 12 | yes | 2t    | 3.05   | 1.38 | 22.174 | -9.83E-02 | -5.75E-02 | 1.00E+00  | 8.27E+00   | 6.35E+00    |  | 4.84E+00 | -4.68E-02 | -3.57E-04 |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | frdm2012 | 32 | 12 | yes | 2t    | 3.20   | 1.44 | 20.398 | -2.07E-02 | -2.05E-02 | 1.00E+00  | 8.00E+00   | 6.66E+00    |  | 4.77E+00 | -1.20E-01 | 1.67E-02  |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | hfb22    | 32 | 12 | yes | 2t    | 3.40   | 1.51 | 23.412 | -2.44E-01 | -2.71E-01 | 1.00E+00  | 1.01E+01   | 6.24E+00    |  | 4.55E+00 | -1.30E-01 | 4.68E-02  |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | ktyu     | 32 | 12 | yes | 2t    | 3.68   | 1.60 | 20.707 | -3.13E-02 | 1.79E-01  | 1.24E+00  | 8.61E+00   | 6.81E+00    |  | 5.19E+00 | 2.30E-02  | -2.19E-02 |
| 124Xe | 124 | 54 | 29-Aug | Tmean  | tuyy     | 32 | 12 | yes | 2t    | 4.30   | 1.78 | 21.222 | 1.25E-01  | -2.58E-02 | 1.79E+00  | 8.03E+00   | 6.24E+00    |  | 5.18E+00 | -1.64E-01 | 3.36E-02  |
|       |     |    |        |        |          |    |    |     |       |        |      |        |           |           |           |            |             |  |          |           |           |
|       |     |    |        |        |          |    |    |     |       | meanW  |      | 21.238 | -0.125    | 0.007     |           | 8.783      | 6.579       |  | 4.978    | -0.109    | 0.013     |
|       |     |    |        |        |          |    |    |     |       | sigmaW |      | 0.366  | 0.042     | 0.048     |           | 0.231      | 0.108       |  | 0.082    | 0.024     | 0.007     |

| Line        | Last | chi2<br>local | LogDif<br>local | chi2<br>total | LogDif<br>total |
|-------------|------|---------------|-----------------|---------------|-----------------|
| <b>Z=48</b> | 40   | 1             | 5               | 0.5           | 8               |

|        | e1     | e2    | AA-factor | Tlim<br>50 | Tlim<br>150 |  | dRauto 0 | dRauto 1 | dRauto 2 |
|--------|--------|-------|-----------|------------|-------------|--|----------|----------|----------|
| meanW  | -0.134 | 0.022 |           | 8.888      | 6.090       |  | 5.152    | -0.105   | 0.01812  |
| sigmaW | 0.009  | 0.019 |           | 0.128      | 0.229       |  | 0.179    | 0.009    | 0.012    |

e2 ( $k_{\text{ZN}}$ ) – can be ignored

| RESULT -product |          |    |    |     |       |         |      |        |
|-----------------|----------|----|----|-----|-------|---------|------|--------|
| method          | mass     | NP | s  | 2p  | mw/2t | product | wErr | weight |
| Tmean           | hfb27    | 32 | 12 | yes | 2t    | 10.93   | 1.00 | 1.000  |
| Tmean           | frdm2012 | 32 | 12 | yes | 2t    | 11.70   | 1.18 | 0.723  |
| Tmean           | ws4rbf   | 32 | 10 | yes | 2t    | 16.75   | 1.98 | 0.256  |
| Tmean           | tuyy     | 32 | 12 | yes | 2t    | 17.66   | 2.09 | 0.229  |
| Tmean           | ame2020  | 32 | 12 | yes | 2t    | 23.09   | 2.66 | 0.141  |
| Tmean           | unedf1   | 32 | 12 | yes | 2t    | 28.07   | 3.09 | 0.105  |
| Tmean           | ktyu     | 32 | 12 | yes | 2t    | 28.97   | 3.17 | 0.100  |
| Tmean           | hfb22    | 32 | 12 | yes | 2t    | 29.47   | 3.20 | 0.097  |

## A practical form that matches your plot

Baseline (your V1):

$$\varepsilon_0(A) = 13.5 \left( \frac{A}{40} \right)^{1/3} \text{ MeV per abraded}$$

Optional, mild isospin tilt (captures the proton-rich vs neutron-rich trend seen in BeAGLE/INCL):

$$\varepsilon(A, Z) = \varepsilon_0(A) [1 + c I], \quad I = \frac{N-Z}{A}$$

- $c$  is small (typ. 0–0.3). Fit  $c$  once to your compiled BeAGLE/INCL + data; it will be close to zero for near-stability projectiles and grows slightly for more neutron-rich beams. (If you don't want any  $Z$ -dependence, set  $c = 0$  and you're exactly on the purple V1 curve.)

Then

$$E^*(A, Z; \Delta A) = \varepsilon(A, Z) \Delta A.$$

## Example: predict for a proton-rich $^{92}\text{Mo}$ beam

$$A = 92, Z = 42, N = 50, I = \frac{8}{92} = 0.087.$$

- Without isospin term (your V1 only):

$$\varepsilon_0(92) = 13.5 \left( \frac{92}{40} \right)^{1/3} \approx \mathbf{17.82 \text{ MeV/abraded.}}$$

- With a modest isospin correction (say  $c = 0.2$ ):

$$\varepsilon(92, 42) \approx 17.82 \times (1 + 0.2 \times 0.087) \approx \mathbf{18.13 \text{ MeV/abraded.}}$$

## Notation

- $A^{1/3}$  baseline (your V1):  $f(A) = \left( \frac{A}{40} \right)^{1/3}$ .
- Asymmetry  $I = (N - Z)/A$ .
  - $I_{78} = \frac{6}{78} = 0.076923$ ,  $I_{124} = \frac{16}{124} = 0.129032$ ,  $I_{92} = \frac{8}{92} = 0.086957$ .
- Measured (from your table, per mass model):
  - $y_{78} \equiv e0(^{78}\text{Kr}) (\approx 12\text{--}13)$
  - $y_{124} \equiv e0(^{124}\text{Xe}) (\approx 21\text{--}22)$

## Model (what I suggested)

$$\varepsilon(A, Z) = k f(A) [1 + c I]$$

- $k$  is the overall scale (your "e0 at  $A = 40$ " in effect),
- $c$  is a small dimensionless **isospin tilt** (your "e1").

## Solve $k, c$ for each mass model (from the two beams)

Let  $a = f(78)$ ,  $b = f(124)$  (numerically  $a = 1.249333$ ,  $b = 1.458100$ ).

1. Compute

$$r = \frac{y_{124}}{y_{78}} \cdot \frac{a}{b}$$

2. Then

$$c = \frac{1 - r}{r I_{78} - I_{124}},$$

$$k = \frac{y_{78}}{a (1 + c I_{78})}$$

## Predict for $^{92}\text{Mo}$ ( $A=92, Z=42$ )

Let  $f_{92} = f(92) = 1.333454$  and  $I_{92} = 0.086957$ :

$$e0(^{92}\text{Mo}) = \varepsilon_{92} = k f_{92} (1 + c I_{92})$$

# How to get Excitation energy parameter for $^{92}\text{Mo}$

78Kr\_124Xe.xlsx

| Sum of e0      |        |        | Column Labels |         |      | e0      |         |
|----------------|--------|--------|---------------|---------|------|---------|---------|
|                |        |        | 78Kr          | 124Xe   |      | 92Mo    | 144Sm   |
|                |        |        | 78            | 124     |      | 92      | 144     |
| Row Labels     |        |        | 36            | 54      | R    | 42      | 62      |
| ame2020        | 12.668 | 22.174 |               |         | 0.67 | 14.673  | 24.776  |
| frdm2012       | 11.994 | 20.398 |               |         | 0.69 | 13.788  | 22.713  |
| hfb22          | 13.288 | 23.412 |               |         | 0.66 | 15.417  | 26.180  |
| hfb27          | 12.941 | 20.76  |               |         | 0.73 | 14.659  | 22.946  |
| ktyu           | 12.336 | 20.707 |               |         | 0.70 | 14.134  | 23.020  |
| tuyy           | 13.051 | 21.222 |               |         | 0.72 | 14.833  | 23.498  |
| unedf1         | 14.136 | 21.719 |               |         | 0.76 | 15.846  | 23.867  |
| ws4rbf         | 13.083 | 20.148 |               |         | 0.76 | 14.674  | 22.148  |
| Isospin factor |        |        | 0.0769        | 0.1290  |      | 0.0870  | 0.1389  |
| fA             |        |        | 1.24933       | 1.45810 |      | 1.32001 | 1.53262 |

| Sum of e1  |        |        | Column Labels |       |          | e1        |           |
|------------|--------|--------|---------------|-------|----------|-----------|-----------|
|            |        |        | 78Kr          | 124Xe |          | 92Mo      | 144Sm     |
|            |        |        | 78            | 124   |          | 92        | 144       |
| Row Labels |        |        | 36            | 54    | K        | 42        | 62        |
| ame2020    | 0.038  | -0.098 |               |       | -3.0E-03 | -3.40E-03 | -1.58E-01 |
| frdm2012   | -0.253 | -0.021 |               |       | 2.6E-03  | -2.16E-01 | -7.88E-02 |
| hfb22      | -0.081 | -0.244 |               |       | -1.3E-03 | -9.96E-02 | -1.68E-01 |
| hfb27      | -0.100 | -0.261 |               |       | -1.3E-03 | -1.18E-01 | -1.86E-01 |
| ktyu       | 0.007  | -0.031 |               |       | -3.1E-04 | 2.72E-03  | -1.34E-02 |
| tuyy       | -0.089 | 0.125  |               |       | 1.7E-03  | -6.46E-02 | 2.49E-02  |
| unedf1     | -0.348 | -0.131 |               |       | 1.7E-03  | -3.23E-01 | -2.32E-01 |
| ws4rbf     | -0.108 | -0.102 |               |       | 5.0E-05  | -1.08E-01 | -1.05E-01 |

# Average-Weighted result

92Mo\_summary2.xlsm

Z=36, N=32

Working in log-space

Regular average

Weighted average

Asymmetric Weighted average

Final result in linear space

| wErr            | 1.000         | 1.176    | 1.978    | 2.090    | 2.660    | 3.093    | 3.165    | 3.205    |   | count    | average | stDev    | averageW | sigmaW   | asym   | asym er-min | asym err-plus | CS       | dCS-     | dCS+ |
|-----------------|---------------|----------|----------|----------|----------|----------|----------|----------|---|----------|---------|----------|----------|----------|--------|-------------|---------------|----------|----------|------|
| weight          | 1.000         | 0.723    | 0.256    | 0.229    | 0.141    | 0.105    | 0.100    | 0.097    |   |          |         |          |          |          |        |             |               |          |          |      |
| err             | 0.1           | 0.1      | 0.1      | 0.1      | 0.1      | 0.1      | 0.1      | 0.1      |   |          |         |          |          |          |        |             |               |          |          |      |
| Sum of logValue | Column Labels |          |          |          |          |          |          |          |   |          |         |          |          |          |        |             |               |          |          |      |
| Row Labels      | ame2020       | frdm2012 | hfb22    | hfb27    | ktyu     | tuyy     | unedf1   | ws4rbf   |   |          |         |          |          |          |        |             |               |          |          |      |
| 36032           | -11.2124      | -9.4153  | -11.1029 | -10.9287 | -11.4284 | -11.1956 | -8.7143  | -12.0695 | 8 | -10.7584 | 1.0425  | -10.6354 | 0.3424   | -10.6362 | 0.6767 | 0.9831      | 2.31E-11      | 1.82E-11 | 1.99E-10 |      |
| 36033           | -9.4572       | -7.8130  | -8.9366  | -8.0534  | -9.2344  | -7.6570  | -6.9229  | -9.3183  | 8 | -8.4241  | 0.8760  | -8.6538  | 0.3074   | -8.8552  | 0.6605 | 0.8806      | 1.40E-09      | 1.09E-09 | 9.21E-09 |      |
| 36034           | -7.9198       | -6.2975  | -7.1237  | -7.7824  | -7.2311  | -7.6533  | -5.6909  | -7.4676  | 8 | -7.1458  | 0.7254  | -7.2409  | 0.2784   | -7.3577  | 0.6225 | 0.8565      | 4.39E-08      | 3.34E-08 | 2.72E-07 |      |
| 36035           | -5.4290       | -4.5121  | -5.2342  | -5.1552  | -5.3199  | -5.5366  | -4.1907  | -5.2961  | 8 | -5.0842  | 0.4440  | -5.0834  | 0.1601   | -5.1208  | 0.3437 | 0.4905      | 7.57E-06      | 4.14E-06 | 1.59E-05 |      |
| 36036           | -3.2756       | -2.9083  | -2.9701  | -4.2258  | -3.4554  | -3.8397  | -3.2157  | -3.8470  | 8 | -3.4672  | 0.4356  | -3.2786  | 0.1465   | -3.1883  | 0.2984 | 0.2311      | 6.48E-04      | 3.22E-04 | 4.55E-04 |      |
| 36037           | -1.9324       | -1.6059  | -1.7057  | -2.1497  | -1.9316  | -2.3697  | -1.7792  | -1.7183  | 8 | -1.8991  | 0.2390  | -1.8438  | 0.0760   | -1.8302  | 0.1548 | 0.1836      | 1.48E-02      | 4.43E-03 | 7.78E-03 |      |
| 36038           | -0.9234       | -0.6479  | -0.6035  | -1.2739  | -1.0352  | -1.3781  | -0.9113  | -1.0194  | 8 | -0.9741  | 0.2523  | -0.8746  | 0.0828   | -0.8414  | 0.1607 | 0.1697      | 1.44E-01      | 4.46E-02 | 6.89E-02 |      |
| 36039           | 0.0096        | 0.2285   | 0.1347   | 0.1217   | 0.0753   | -0.1141  | 0.1608   | 0.1818   | 8 | 0.0998   | 0.1020  | 0.1017   | 0.0377   | 0.0874   | 0.0946 | 0.1182      | 1.22E+00      | 2.39E-01 | 3.82E-01 |      |
| 36040           | 0.5642        | 0.6765   | 0.8021   | 1.2261   | 0.3143   | 0.7476   | 0.7236   | 1.2743   | 8 | 0.7911   | 0.3002  | 0.7010   | 0.0863   | 0.6318   | 0.0950 | 0.1776      | 4.28E+00      | 8.42E-01 | 2.16E+00 |      |
| 36041           | 1.1360        | 1.0849   | 0.8176   | 1.2020   | 1.1947   | 1.1516   | 1.2013   | 1.3382   | 8 | 1.1408   | 0.1401  | 1.1107   | 0.0415   | 1.1122   | 0.0918 | 0.0571      | 1.29E+01      | 2.47E+00 | 1.82E+00 |      |
| 36042           | 1.6154        | 1.2313   | 1.4885   | 1.3016   | 1.1926   | 1.2271   | 1.2768   | 1.2656   | 8 | 1.3249   | 0.1385  | 1.4079   | 0.0671   | 1.4706   | 0.2047 | 0.1615      | 2.96E+01      | 1.11E+01 | 1.33E+01 |      |
| 36043           | 1.0930        | 1.2330   | 1.0521   | 1.1285   | 1.1226   | 1.0780   | 1.1263   | 1.1362   | 8 | 1.1212   | 0.0503  | 1.1342   | 0.0242   | 1.1365   | 0.0640 | 0.0837      | 1.37E+01      | 1.88E+00 | 2.91E+00 |      |
| 36044           | 0.9371        | 1.1639   | 1.0838   | 1.0398   | 0.8540   | 0.8449   | 0.7262   | 0.8870   | 8 | 0.9421   | 0.1350  | 1.0042   | 0.0463   | 1.0130   | 0.1008 | 0.1256      | 1.03E+01      | 2.14E+00 | 3.45E+00 |      |
| 36045           | 0.3532        | 0.4538   | 0.3216   | 0.4522   | 0.3639   | 0.2921   | 0.2330   | 0.3395   | 8 | 0.3512   | 0.0701  | 0.3793   | 0.0231   | 0.3851   | 0.0564 | 0.0667      | 2.43E+00      | 2.96E-01 | 4.03E-01 |      |
| 36046           | -0.0212       | -0.0336  | -0.2092  | 0.6936   | -0.1242  | -0.0965  | -0.2261  | -0.0247  | 8 | -0.0052  | 0.2745  | 0.0027   | 0.0840   | -0.0131  | 0.0740 | 0.1795      | 9.70E-01      | 1.52E-01 | 4.97E-01 |      |
| 36047           | -0.7515       | -0.8066  | -0.9230  | -0.7378  | -0.8641  | -0.8367  | -0.9819  | -0.6835  | 8 | -0.8231  | 0.0930  | -0.7974  | 0.0259   | -0.7776  | 0.0642 | 0.0475      | 1.67E-01      | 2.29E-02 | 1.93E-02 |      |
| 36048           | -1.2751       | -1.3499  | -1.5408  | -1.4438  | -1.5582  | -1.4943  | -1.6816  | -1.4259  | 8 | -1.4712  | 0.1189  | -1.3803  | 0.0430   | -1.3217  | 0.0986 | 0.0618      | 4.77E-02      | 9.68E-03 | 7.29E-03 |      |
| 36049           | -2.4407       | -2.5264  | -2.7399  | -2.4614  | -2.4512  | -2.4147  | -2.6140  | -2.3917  | 8 | -2.5050  | 0.1104  | -2.4990  | 0.0349   | -2.4801  | 0.0895 | 0.0572      | 3.31E-03      | 6.16E-04 | 4.66E-04 |      |
| 36050           | -3.8823       | -3.6445  | -4.2062  | -3.6739  | -3.7614  | -3.7710  | -4.0167  | -3.7533  | 8 | -3.8387  | 0.1772  | -3.8201  | 0.0632   | -3.8127  | 0.1394 | 0.1417      | 1.54E-04      | 4.23E-05 | 5.94E-05 |      |
| 37031           | -13.5459      | -12.2580 | -15.0838 | -13.5787 | -13.2272 | -14.0641 | -11.6836 | -6.2325  | 8 | -12.4592 | 2.5471  | -13.0104 | 0.5982   | -13.1558 | 0.7004 | 1.0308      | 6.99E-14      | 5.59E-14 | 6.80E-13 |      |
| 37032           | -12.8150      | -11.4233 | -13.5927 | -12.9762 | -13.4145 | -13.2025 | -10.6594 | -13.8294 | 8 | -12.7391 | 1.0433  | -12.5276 | 0.3261   | -12.4223 | 0.6016 | 0.8094      | 3.78E-13      | 2.84E-13 | 2.06E-12 |      |
| 37033           | -10.9077      | -9.5353  | -11.2279 | -9.8677  | -10.8634 | -10.5377 | -8.7854  | -10.9498 | 8 | -10.3344 | 0.7971  | -10.3791 | 0.2707   | -10.4483 | 0.5521 | 0.7551      | 3.56E-11      | 2.56E-11 | 1.67E-10 |      |
| 37034           | -9.9019       | -8.5199  | -10.0951 | -9.7625  | -9.7424  | -9.5255  | -7.5585  | -10.0172 | 8 | -9.3904  | 0.8326  | -9.4241  | 0.2705   | -9.4602  | 0.5236 | 0.7686      | 3.47E-10      | 2.43E-10 | 1.69E-09 |      |
| 37035           | -7.6965       | -6.6955  | -8.0847  | -6.0140  | -7.5266  | -7.5076  | -5.8801  | -6.1475  | 8 | -6.9441  | 0.8076  | -7.1737  | 0.2603   | -7.3272  | 0.4563 | 0.6287      | 4.71E-08      | 3.06E-08 | 1.53E-07 |      |
| 37036           | -5.8866       | -5.0756  | -6.1022  | -5.5173  | -5.8085  | -6.0967  | -4.7795  | -5.7381  | 8 | -5.6256  | 0.4463  | -5.6113  | 0.1553   | -5.6258  | 0.3210 | 0.4446      | 2.37E-06      | 1.24E-06 | 4.22E-06 |      |
| 37037           | -2.9210       | -3.1952  | -4.2654  | -3.0457  | -3.1888  | -3.4280  | -3.2336  | -2.4789  | 8 | -3.2196  | 0.4752  | -3.1660  | 0.1516   | -3.0674  | 0.3531 | 0.1747      | 8.56E-04      | 4.76E-04 | 4.24E-04 |      |
| 37038           | -2.4209       | -1.8875  | -2.4895  | -2.6423  | -2.1789  | -2.7114  | -2.1648  | -2.1235  | 8 | -2.3273  | 0.2658  | -2.2791  | 0.1031   | -2.2613  | 0.2168 | 0.2969      | 5.48E-03      | 2.15E-03 | 5.38E-03 |      |
| 37039           | -0.7757       | -0.6092  | -1.1769  | -0.9158  | -0.6320  | -0.7595  | -0.8949  | -0.4935  | 8 | -0.7822  | 0.2008  | -0.7669  | 0.0647   | -0.7414  | 0.1395 | 0.1141      | 1.81E-01      | 4.98E-02 | 5.45E-02 |      |
| 37040           | -0.1902       | -0.0346  | -0.0107  | -0.2372  | -0.0746  | -0.1858  | -0.1687  | -0.0032  | 8 | -0.1131  | 0.0865  | -0.1205  | 0.0318   | -0.1341  | 0.0754 | 0.0939      | 7.34E-01      | 1.17E-01 | 1.77E-01 |      |
| 37041           | 0.5837        | 0.7689   | 0.1731   | 0.3641   | 0.6967   | 0.5895   | 0.7575   | 0.6291   | 8 | 0.5703   | 0.1919  | 0.5901   | 0.0672   | 0.6209   | 0.1500 | 0.1231      | 4.18E+00      | 1.22E+00 | 1.37E+00 |      |
| 37042           | 0.9316        | 1.0878   | 1.7447   | 0.9299   | 0.9537   | 0.9509   | 1.0129   | 0.9848   | 8 | 1.0745   | 0.2580  | 1.0594   | 0.0882   | 1.0124   | 0.0977 | 0.2150      | 1.03E+01      | 2.07E+00 | 6.59E+00 |      |
| 37043           | 1.2529        | 1.3989   | 1.0674   | 1.1877   | 1.3001   | 1.2703   | 1.3311   | 1.3029   | 8 | 1.2639   | 0.0937  | 1.2772   | 0.0366   | 1.2902   | 0.0860 | 0.0926      | 1.95E+01      | 3.51E+00 | 4.64E+00 |      |
| 37044           | 1.2035        | 1.3993   | 1.2407   | 1.3228   | 1.2700   | 1.2412   | 1.2446   | 1.1308   | 8 | 1.2566   | 0.0743  | 1.2747   | 0.0323   | 1.2700   | 0.0824 | 0.1084      | 1.86E+01      | 3.22E+00 | 5.28E+00 |      |
| 37045           | 0.9788        | 1.2127   | 0.9751   | 0.9788   | 1.1018   | 0.9972   | 1.0681   | 1.1497   | 8 | 1.0578   | 0.0848  | 1.0592   | 0.0390   | 1.0540   | 0.0939 | 0.1303      | 1.13E+01      | 2.20E+00 | 3.96E+00 |      |
| 37046           | 0.6985        | 0.7680   | 0.7078   | 0.7551   | 0.7475   | 0.6844   | 0.5678   | 0.6826   | 8 | 0.7015   | 0.0592  | 0.7198   | 0.0166   | 0.7218   | 0.0471 | 0.0516      | 5.27E+00      | 5.41E-01 | 6.64E-01 |      |
| 37047           | 0.2188        | 0.2635   | -0.0055  | 0.0536   | 0.2284   | 0.1242   | 0.1162   | 0.2637   | 8 | 0.1579   | 0.0945  | 0.1897   | 0.0332   | 0.2180   | 0.0838 | 0.0506      | 1.65E+00      | 2.90E-01 | 2.04E-01 |      |

| Name             | Ext   | Size   | ↓Date            |
|------------------|-------|--------|------------------|
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| [238U]           | <DIR> |        | 11/04/2023 02:08 |
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| 92Mo_C_BAA       | cs    | 27,785 | 09/22/2025 17:27 |
| 124Xe_Be_345AMeV | cs    | 4,259  | 06/01/2025 01:30 |
| 136Xe_Be_1AGeV   | cs    | 3,180  | 05/30/2025 23:24 |
| 78Kr_Be_345AMeV  | cs    | 21,489 | 05/30/2025 18:25 |
| 129Xe_Al_790AMeV | cs    | 5,883  | 01/23/2021 23:04 |
| 82Se_Be_140AMeV  | cs    | 8,994  | 12/26/2013 12:44 |

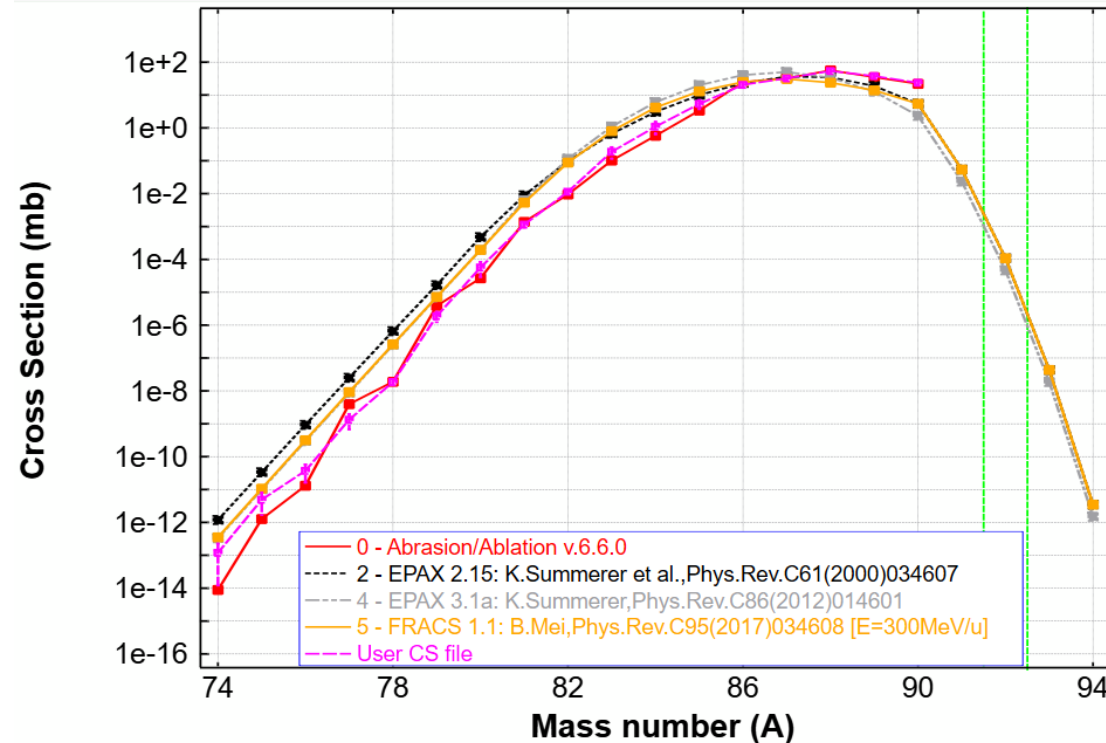
Result of this analysis

Experimental CS  
used in this analysis

## Cross sections (Projectile Fragmentation)

<sup>92</sup>Mo + C → Z=40

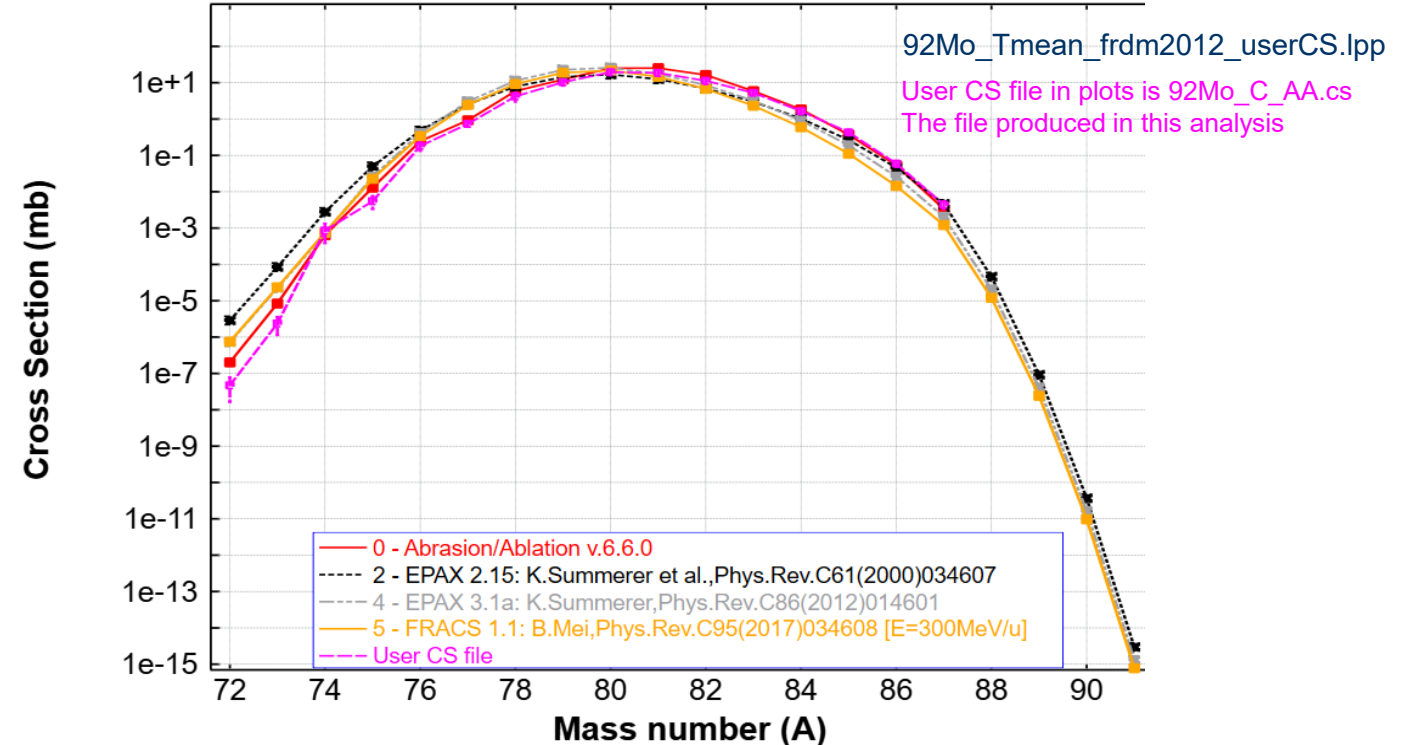
E\* method: <3>; <T>: 13.79(-0.22,0.00) MeV; No Intrin.Thermalztn; LimitTemp: No; DB<sub>i</sub>=FRDM2012  
NP=32; SE: "DB1+Cal1"; Den: "auto"; GeomCor: "On"; Tunlg: "auto"; FisBar= #1; BarFac= 1.00; Modes=1011 1000 010



## Cross sections (Projectile Fragmentation)

<sup>92</sup>Mo + C → Z=37

E\* method: <3>; <T>: 13.79(-0.22,0.00) MeV; No Intrin.Thermalztn; LimitTemp: No; DB<sub>i</sub>=FRDM2012  
NP=32; SE: "DB1+Cal1"; Den: "auto"; GeomCor: "On"; Tunlg: "auto"; FisBar= #1; BarFac= 1.00; Modes=1011 1000 010



## Title

“Weighted AA Ensemble Cross Sections”  
 “Model-averaged AA Predictions”  
 “Model-averaged AA cross sections”  
 “Benchmark-weighted AA cross sections”

## Neutral/statistical

Weighted AA average cross sections  
 Model-averaged AA cross sections  
 Weighted model AA cross sections  
 AA cross sections from weighted model averaging (WMA)

## Physics-oriented

Benchmark-calibrated AA cross sections  
 Reference-weighted AA cross sections  
 Data-guided AA average cross sections  
 AA cross sections with mass-model weighting

## Slightly more formal

Weighted synthesis of AA cross sections  
 Aggregated AA predictions  
 Composite AA cross sections  
 Weighted AA estimate

## 1. Common practice vs new

### •Common practice pieces:

- Calibrating AA parameters on one or two reference beams is standard.
- Comparing several mass models (FRDM, HFB, KTUY, WS4, ...) is very common.
- Assigning weights based on  $\chi^2$  performance has been done in some mass-model systematics papers, usually under the name “weighted model average” or “Bayesian model averaging.”

### •Less common / novel piece:

- In fragmentation cross-section systematics, most groups either (i) show a *band/spread* of different mass models, or (ii) pick one “best” mass model.
- Using *quantitative weights from multiple reference beams* to produce a single averaged AA prediction with propagated uncertainties is much less common.
- To my knowledge, this kind of weighted AA cross-section ensemble has **not yet appeared systematically in PRC/EPJA fragmentation papers.**

So you are not reinventing statistics, but you are **bringing an established idea (model averaging) into nuclear fragmentation systematics**, which makes it publishable.

## 2. Is it publishable?

Yes — absolutely:

- Referees will appreciate that you **do not cherry-pick one mass model**, but instead combine them transparently, with weights tied to real data.
- It gives **more robust extrapolations** to beams where no data exist.
- By publishing, you set a precedent: future groups can compare to your “ensemble AA” rather than debating mass-model choice.

The key will be to **emphasize**:

- The method is *data-driven* (fits to 78Kr and 124Xe).
- It *quantifies model uncertainty* via weighted variance.
- It produces a *single recommended cross section with error bar*.

That is valuable for experimental planning (where people need one number + error, not eight).

Bayesian model averaging (BMA) is exactly the “family resemblance” of what you already do with  $\chi^2$ -based weights. Let me unpack it carefully for your AA cross-section context.

## Bayesian Model Averaging (BMA) for Abrasion–Ablation Cross Sections

### 1. General Bayesian model averaging (BMA)

Suppose you have several models  $M_i$  (here: eight mass models + AA fits). In Bayesian statistics, each model has a posterior probability given the data  $D$ :

$$P(M_i|D) \propto P(D|M_i) P(M_i)$$

where

- $P(D|M_i)$  is the marginal likelihood (how well model  $M_i$  explains the data),
- $P(M_i)$  is the prior probability of model  $i$ .

The final prediction for an observable  $y$  is the model-averaged posterior predictive distribution:

$$P(y|D) = \sum_i P(y|M_i, D) P(M_i|D).$$

### 2. Connection to current approach

Your weights

$$w_i \propto 1 / (\chi_{78\text{Kr},i}^2 \times \chi_{124\text{Xe},i}^2)$$

are a frequentist proxy for  $P(M_i|D)$ . In full Bayesian form, you would instead compute  $P(D|M_i) \propto \exp(-\chi_i^2/2)$ , assuming Gaussian residuals. Then  $w_i = \exp(-\chi_i^2/2) / \sum_j \exp(-\chi_j^2/2)$ .

### 3. Bayesian version for AA analysis

1. Model prior: assume equal priors for all eight mass models.
2. Likelihood: for each model, compute  $L_i = \exp(-\chi_{78\text{Kr},i}^2/2) \times \exp(-\chi_{124\text{Xe},i}^2/2)$ .
3. Posterior weight:  $w_i = L_i / \sum_j L_j$ .
4. Model-averaged prediction:  $\langle \sigma \rangle = \sum_i w_i \sigma_i$ , with uncertainty from the posterior variance.

### 4. Advantages vs $\chi^2$ -based weights

- Theoretical grounding: weights correspond to probabilities.
- Automatic scaling: exponential likelihood prevents overweighting mediocre fits.
- Error bars: BMA naturally propagates both within-model error and between-model spread.

### 5. Suggested manuscript wording

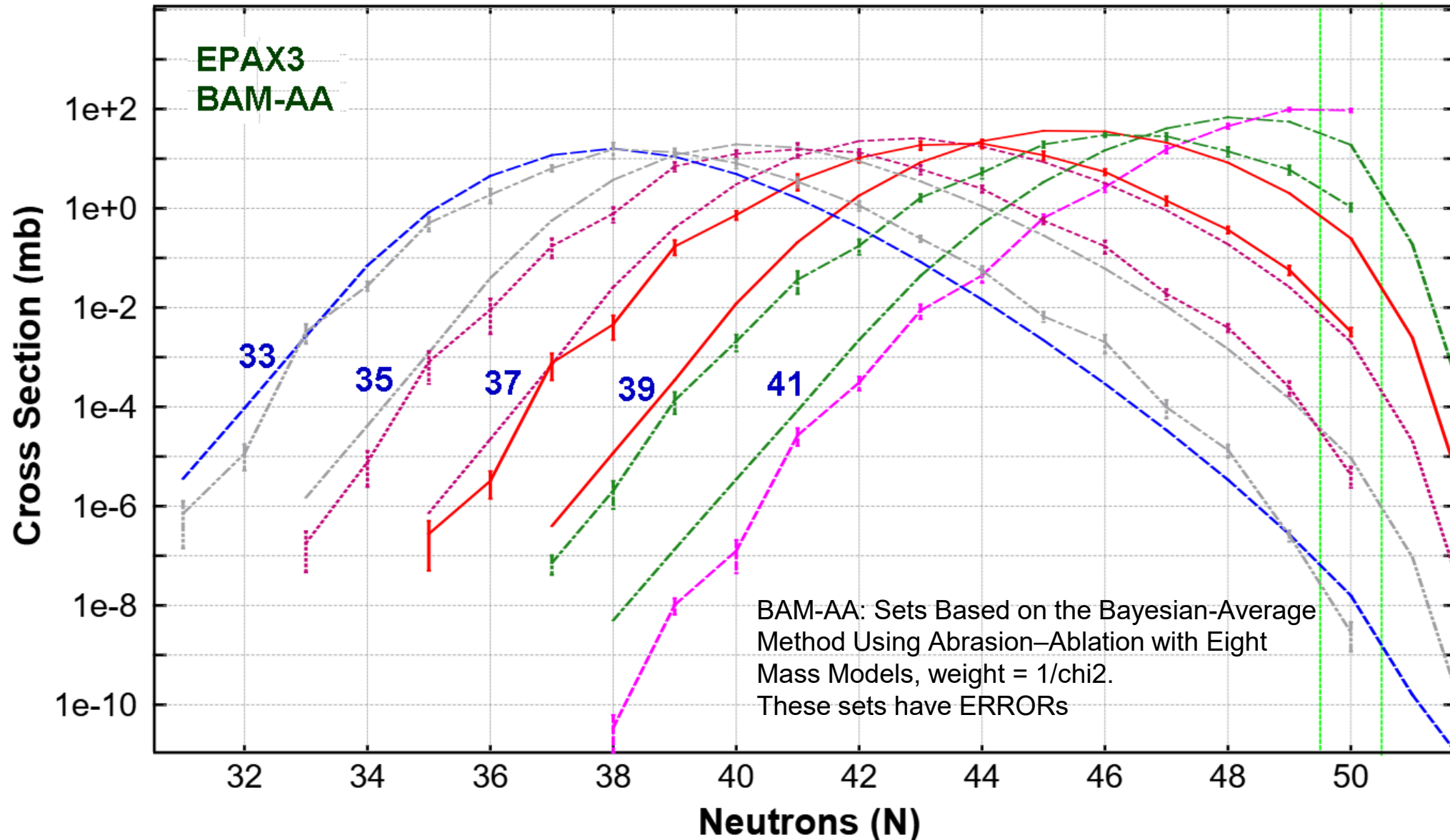
We employed a weighted model averaging procedure, akin to Bayesian model averaging, to combine AA predictions based on eight nuclear mass models. In this framework, the weight of each mass model is proportional to the likelihood of reproducing the benchmark cross sections ( $^{78}\text{Kr}$  and  $^{124}\text{Xe}$ ), effectively assigning posterior probabilities to each model. The final deduced cross sections thus represent a model-averaged prediction with uncertainties reflecting both experimental input and inter-model spread.

**$^{92}\text{Mo}$**

**Cross sections (Projectile Fragmentation)**

$^{92}\text{Mo} (140 \text{ MeV/u}) + \text{C} \rightarrow \text{Z}=41$

NP=32; SE: "DB1+Cal1"; Den: "auto"; GeomCor: "On"; Tunlg: "auto";  $\text{FisBar}=\#1$ ;  $\text{Bar}^{\text{Fac}}=1.00$ ; Modes= $^{1011} 1000 010$

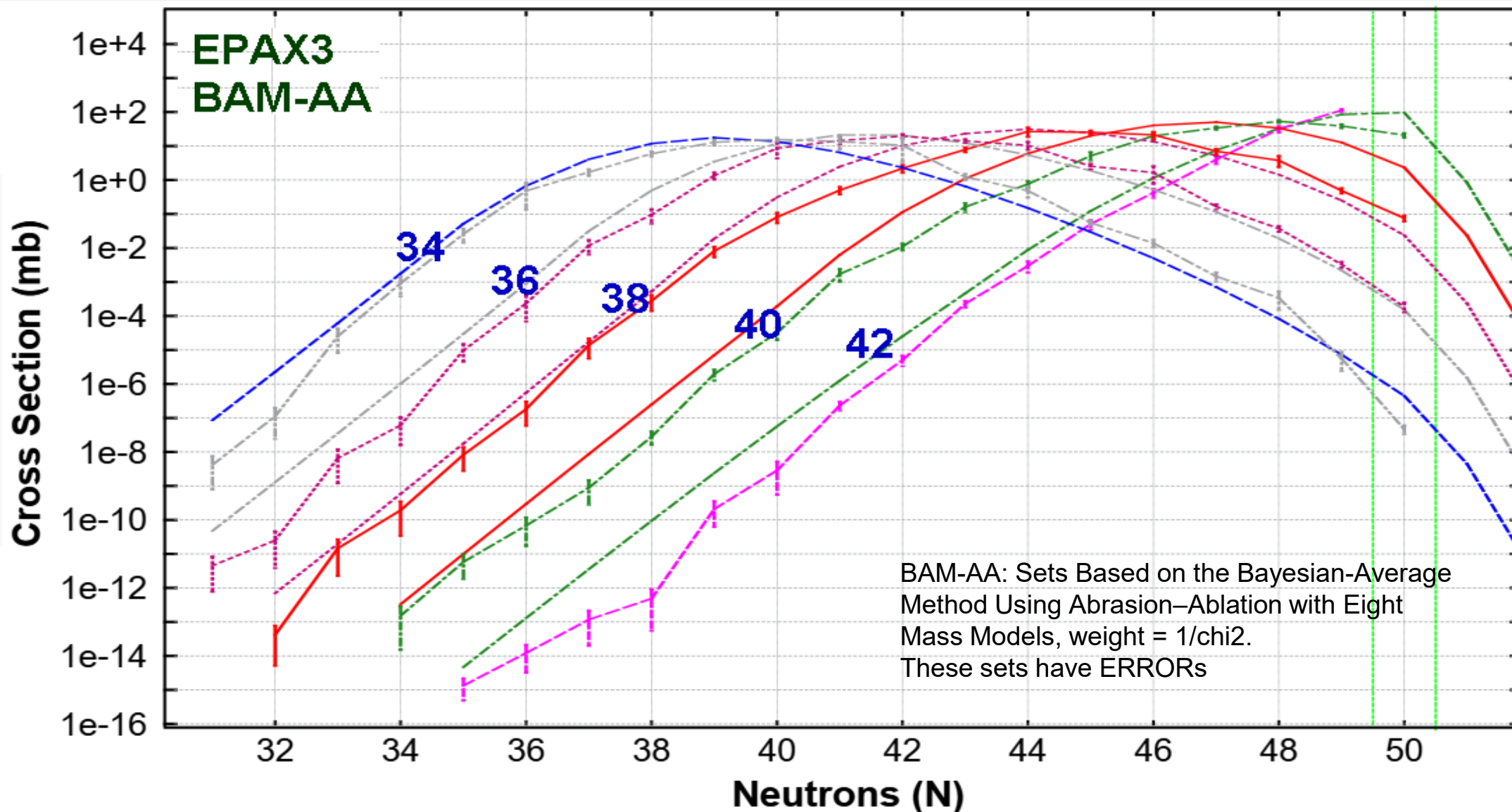


## $^{92}\text{Mo}$

### Cross sections (Projectile Fragmentation)

$^{92}\text{Mo}$  (140 MeV/u) + C  $\rightarrow$  Z=42

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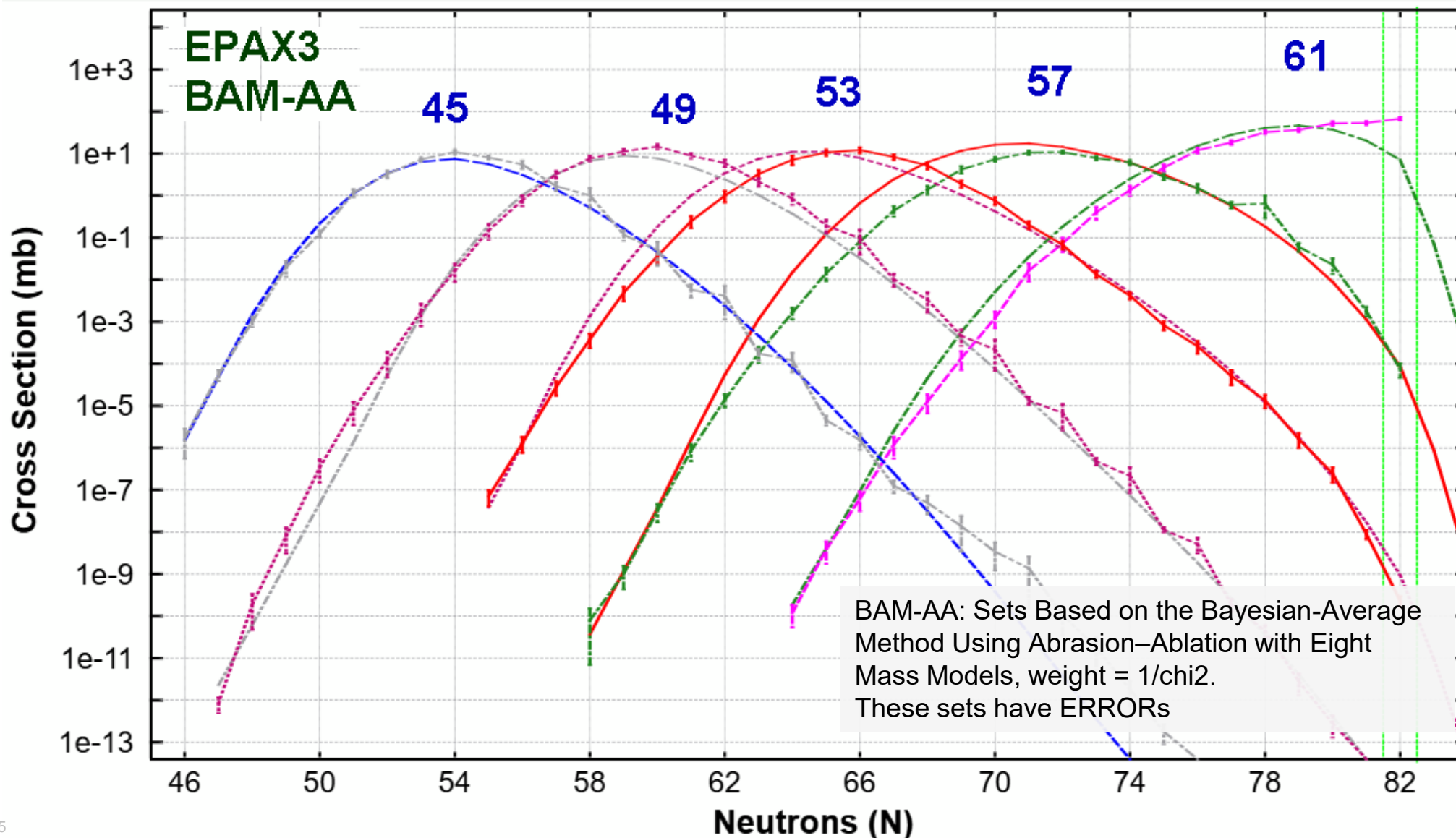


## $^{144}\text{Sm}$

### Cross sections (Projectile Fragmentation)

$^{144}\text{Sm}$  (140 MeV/u) + C  $\rightarrow$  Z=61

NP=32; SE: "DB1+Cal1"; Den: "auto"; GeomCor: "On"; Tunlg: "auto"; FisBar= #1; Bar<sup>Fac</sup>= 1.00; Modes=1011 1000 010 E\* method: <3>;

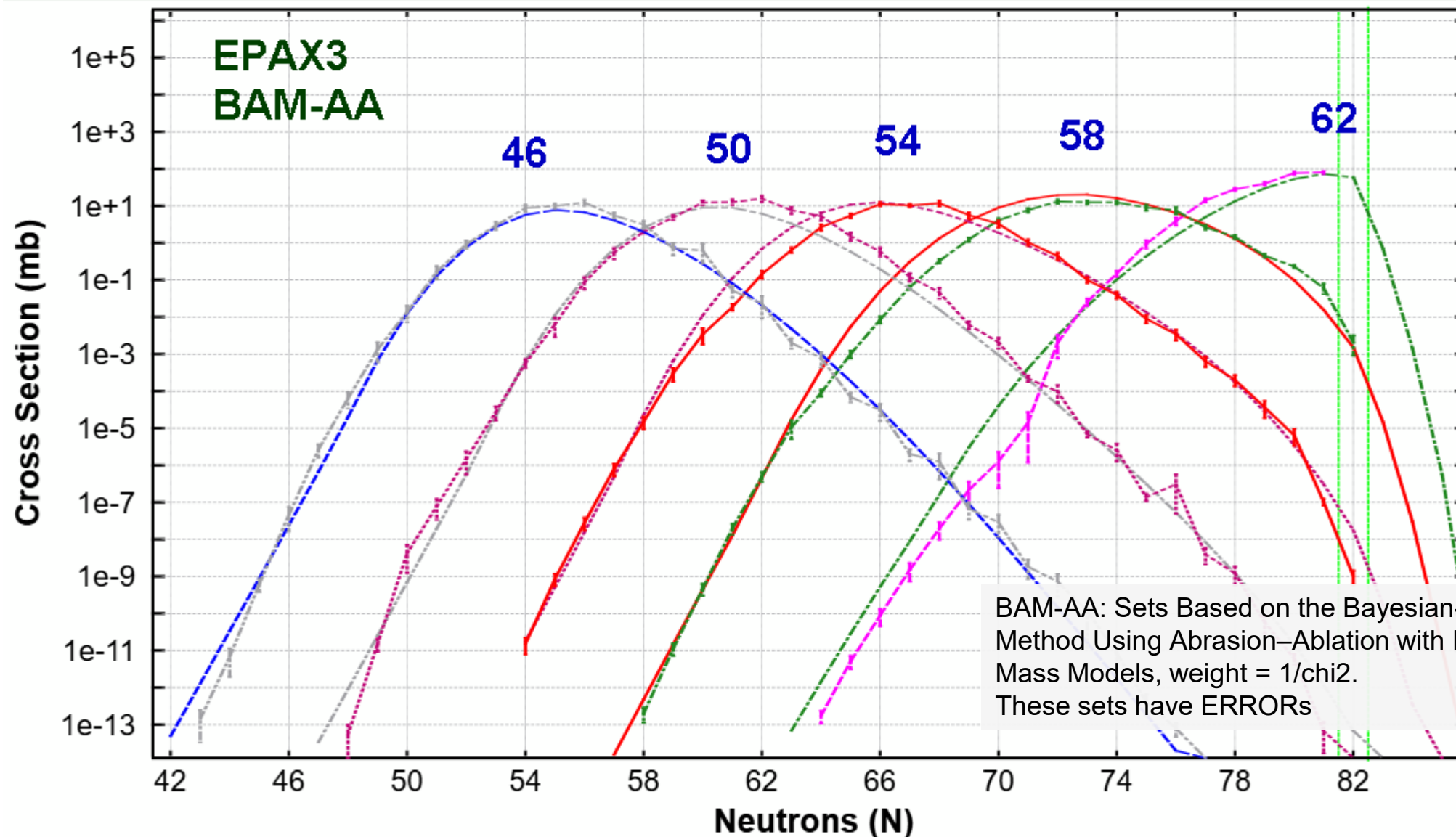


## $^{144}\text{Sm}$

### Cross sections (Projectile Fragmentation)

$^{144}\text{Sm}$  (140 MeV/u) + C  $\rightarrow$  Z=62

NP=32; SE: "DB1+Cal1"; Den: "auto"; GeomCor: "On"; Tunlg: "auto"; FisBar= #1; Bar<sup>Fac</sup>= 1.00; Modes=<sup>1011 1000 010</sup> E\* method: <3>;



BMA + EPAX3 + experimental CS

Coming soon

BMA + EPAX3 + experimental CS

Coming soon